

# Tungsten divertor erosion in all metal devices: lessons from the ITER-like wall of JET and the all tungsten ASDEX Upgrade

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Tungsten erosion has been quantified in the ITER like wall project at JET for the outer divertor and compared with results from the all tungsten ASDEX Upgrade. In L-mode, effective sputtering yields of typically  $10^{-4}$  were measured under attached divertor conditions with divertor plasma temperatures of  $\sim 30$  eV. This value corresponds to a beryllium fraction of 0.5% at the divertor target, a value that was confirmed by spectroscopy, which means that beryllium was the main sputtering species. A signature of prompt redeposition was observed in the analysis of WI 400.9 nm and WII 364 nm line ratios. Inter- and intra-ELM sputtering were compared for an example of 10 Hz ELMs with 13 MW NBI heating, in which intra-ELM sputtering was found to dominate by a factor of 5. Nitrogen seeding was demonstrated to initially increase the tungsten sputtering by a factor of three due to higher extrinsic impurity levels and to have a net beneficial effect by reducing the tungsten sputtering when the divertor plasma temperature was decreased from the initial 25 eV down to 15 eV.

## I. INTRODUCTION

The current design of ITER projects for its active phase tungsten (W) as plasma-facing components (PFCs) in the divertor areas, i.e. the areas receiving the highest particle and energy flux densities. An important issue in this respect remains the physical sputtering of W by impurities, especially when extrinsic impurities are seeded to reduce the power loads on the PFCs. A high local W source in the divertor may cause unduly high W concentrations in the centre, cooling of the plasma and thus deterioration of the fusion performance. In the present work, we utilize the present ITER-like Wall at JET matching the environment for ITER closely to gain insights into relevant aspects of divertor W erosion and W transport into the main plasma. The main ingredients in relation to tungsten sputtering are firstly the identity, the concentration, and the energy of the sputtering particles, secondly the fraction of the sputtered particles that really leaves the surface, i.e., is not promptly redeposited, and thirdly, the efficiency with which the particles reach the core plasma, i.e. divertor screening. The present work will focus on the first two of these aspects.

The approach is to quantify the W erosion in dependence of a wide range of low-Z impurity species, divertor particle flux densities and plasma temperatures and thus to allow for an extrapolation to ITER as well as fusion devices beyond. In particular, spectroscopy is performed on W and W<sup>+</sup> in the ultraviolet and blue spectral region and experimental photon efficiencies from TEXTOR are used to quantify the local W source strength. A consistency analysis is performed by comparing the various spectral lines as well as by placing the source strengths in the context of the spectrally determined impurity species distribution and simple erosion estimates using Bohdan-sky's formula for low-energy ion sputtering, and similar experiments performed at ASDEX Upgrade with its full-W wall. Experiments in H-mode are used to gain insight in the ratio between inter- and intra-ELM sputtering. Finally, impurity seeding is employed to assess the trade-off between introducing more sputtering particles and lowering the impact energy thereof by plasma cooling.

## II. DIAGNOSTICS AND METHODS

Tungsten erosion was quantified by means of passive emission spectroscopy. Several spectroscopic systems were used to monitor the WI line radiation at 400.9 nm at the vertical target in the JET outer divertor. Primarily, a re-designed mirror-link system viewing the tar-

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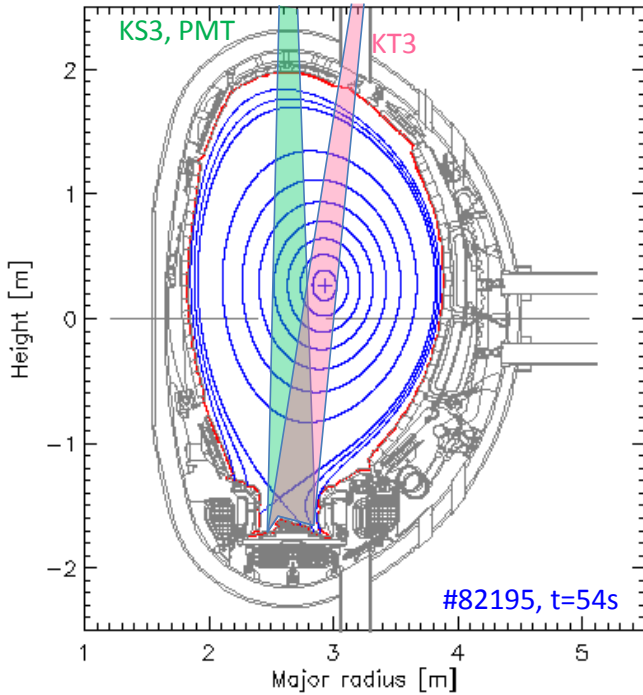


FIG. 1: Cross section of JET in which the lines of sight monitored by the various spectroscopy systems are indicated. The KT3 system covers a chord of 360 mm long and therewith the vertical target plate by 20 lines of sights in a mirror linked system. The KS3 and PMT systems view 10 chords of 20 mm diameter using fiber optics, therewith also covering the vertical target plate.

get from the top of the vessel and analyzing the light in three wavelength ranges with Czerney-Turner spectrometers was used [1], to which we will refer as *KT3*. The system was typically set (unless otherwise stated) to provide every 0.04 s a spectrum covering a wavelength range of 395-409 nm for 20 lines of sight covering 360 mm of the outer divertor. In a second system, the outer divertor area is viewed, again from the top of the vessel, in 10 lines of sight, each covering  $\sim 20$  mm diameter spots at the divertor target, and relayed by fiber optics to Photo Multiplier Tubes equipped with 400.9 nm bandpass filters (1 nm bandwidth), providing a time response of up to 10 kHz (referred to as *PMTs* or to one of four tunable Czerney-Turner spectrometers (referred to as *PMTs* [2]. A schematic of the lines of sight of the three spectroscopic systems is shown in Fig. 1.

The measured light intensities were transformed into tungsten particle flux densities using the number of ionizations per emitted photon [3], i.e. the  $(S/XB)$  value. We used the following formula to incorporate its dependence on the plasma temperature  $T_e$  as was found by recent experiments at the TEXTOR tokamak in combination with experimental results from other devices [4]:

$$\frac{S}{XB}(T_e) = 53.7 \left( 1 - 1.04 \exp \left( -\frac{T_e}{22.1} \right) \right). \quad (1)$$

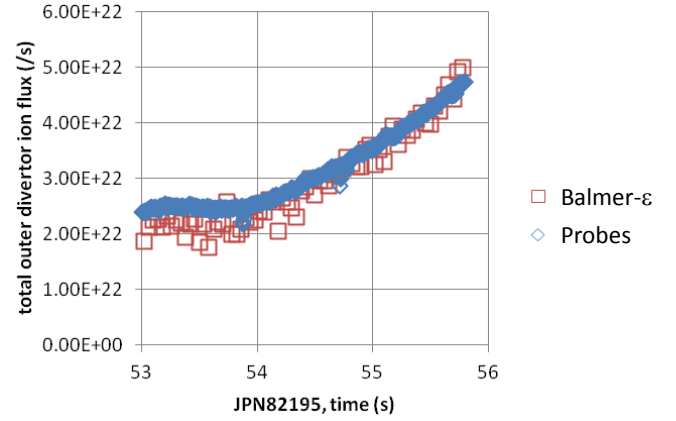


FIG. 2: Comparison of the outer divertor particle flux inferred from Langmuir probe measurements and from Balmer- $\epsilon$  line intensity measurements.

It is noted that generally a constant value of  $(S/XB) = 20$  is used, e.g. by Dux et al.[6]

The same spectroscopy systems and approach were applied to analyze hydrogen and impurity fluxes to the target. The following lines and  $(S/XB)$  values (which were selected to reflect a typical divertor plasma temperature of 20-30 eV, as was encountered in the experiments presented here) were used:

$$\begin{aligned} \text{H}\epsilon \text{ (397 nm): } S/XB &= 1.4 \times 10^4 \\ \text{Be II (527 nm): } S/XB &= 70 \\ \text{C II (515 nm): } S/XB &= 10 \\ \text{C III (465 nm): } S/XB &= 1 \end{aligned} \quad (2)$$

For hydrogen flux calculations, we additionally multiplied the  $S/XB$  value by 2 in order to take the effect of molecules into account [5].

Finally, Langmuir probe measurements were used to determine profiles of the divertor plasma temperature as well as the incident plasma flux densities. The measured saturation currents are projected on a horizontal plane to obtain the normal incident particle flux density. However, the complicated 3D shaping of the individual lamella's of which the vertical target consists, makes that this projected number is not necessarily reflecting the average local normal flux density for the line of sight observed by the spectrometers. Therefore, we performed a consistency check on the integrated outer divertor particle flux inferred from probe measurements and from Balmer epsilon intensity profiles. The result is plotted in Fig. 2 for discharge JPN 82195 and shows that the two approaches agree within 25%.

### III. ASSESSMENT OF THE MAIN SPUTTERING PARTICLE IN L-MODE EXPERIMENTS

The tungsten erosion in the JET outer divertor was evaluated as a function of the divertor electron tempera-

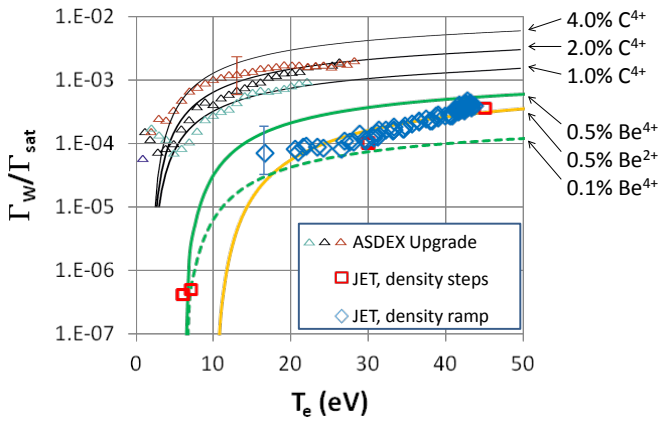


FIG. 3: Effective erosion yields measured in L-mode with 1 MW NBI heating. The yields are compared with data measured in ASDEX Upgrade for sputtering in-between ELMs as well as with the erosion yield for different concentrations and charge states of beryllium and carbon.

ture in L-mode discharges with 1 MW auxiliary heating by neutral beams. Data were obtained from three discharges. One was a scan of the divertor temperature from 43 eV down to 17 eV by means of a scan of the divertor fueling rate (JPN 82195). Two discharges contained each three steps in the divertor density in which the divertor temperature was finally lowered to 7 eV (JPN 81474, JPN 81486). The tungsten particle flux densities at the peak of the profile were normalized to the saturation current measured by Langmuir probes at the same radial position. This number shall be referred to as the “effective” erosion yield, as is common practice, to express that the majority particle (deuterium) is not the sputtering particle. The results are plotted in Fig. 3 as a function of the divertor plasma temperature that was measured by the same probe. For comparison, the sputter yield is indicated for an admixture of different concentrations of  $\text{Be}^{2+}$  (the most abundant charge state for  $20 < T_e < 35$  eV) and  $\text{Be}^{4+}$  (the charge state of beryllium closer to the x-point).

The plot shows that the measured effective erosion yield increases in the temperature range  $15 < T_e < 45$  eV but no threshold behavior is encountered in the data from the density ramp. The pulses with the density steps did achieve the tungsten signal to drop to close to the detection limit. These points are indicative of a threshold behavior that corresponds to  $\text{Be}^{4+}$ . However, it can not be excluded that line blending of the WI 400.9 nm line with a presently unknown spectral line is significant at these low intensities.

It is seen that a fraction of 0.5% beryllium in the target flux density is sufficient to explain the observed tungsten sputter signal. This number is in excellent agreement with the intensity of the BeII 527 nm line as was measured with the PMTs. The signal integrated over the entire vertical target was typically  $1.2 \times 10^{18} \pm 2.4 \times 10^{17}$  photons  $\text{m}^{-2}\text{s}^{-1}$ , which translates (with  $S/XB = 70$ )

into  $8.8 \times 10^{19}$  beryllium atoms  $\text{m}^{-2}\text{s}^{-1}$ . This value corresponds for the actual variation in the target saturation current to a fraction of 0.35% up to 0.50%. It is noted that the fraction of beryllium in the target flux had apparently been lower than the beryllium fraction in the main plasma for these particular discharges. Assuming beryllium as the only impurity in the main plasma, we estimated its concentration from Z-effective, which ranged from 1.2 to 1.4 for the discharges under evaluation. Thus typical Be concentrations in the main plasma were 1.8% - 3.6%.

We thus conclude that sputtering by beryllium only explains the entire observed tungsten sputter rate. This obviously doesn’t necessarily mean that sputtering by other impurities is not important. For the case under evaluation, we therefore assess the contribution of carbon. PMT measurements are available for the CIII 465 nm line and give a  $\sim 8$  times larger integrated intensity for the vertical target compared to the BeII 527 nm line. Multiplied with the respective photon efficiencies of 70 and 1, this implies a factor of 10 lower carbon flux density compared to the beryllium flux density, i.e. a carbon fraction of  $\sim 0.05\%$ , of the total particle flux. Assuming the helium-like charge state of 4+ for the carbon, such a fraction implies that the contribution of carbon to the tungsten sputtering is roughly a factor of 5 lower than the sputtering by beryllium.

Qualitative information, but with more spatial and spectral resolution, was available from the KS3 system. Comparing intensity profiles learned that the spatial profile of the CIII 465 nm line radiation was much wider than for the BeII 527 nm line or e.g. the CII 515 nm, the latter two being more alike. The intensity ratio CII/BeII was 0.6, i.e. a particle flux ratio C/Be of 0.08. These numbers confirm again that sputtering by carbon impurities is negligible compared to sputtering by beryllium.

The error bar drawn in Fig. 3 for the effective erosion yields in JET reflects the two main uncertainties in the analysis: the value of the photon efficiency  $S/XB$  (including the underlying uncertainty in the plasma temperature) and the determination of the plasma flux. Both individual errors are estimated to be 30 – 50%.

Data from the all tungsten ASDEX Upgrade, which have been put in the perspective of sputtering by carbon impurities as a placeholder for all low-Z impurity ions present in the divertor target particle flux, are included for comparison. It shows that the effective tungsten sputter yield in JET under attached divertor conditions is less than one tenth of the values measured in ASDEX Upgrade in-between ELMs at similar plasma temperatures. We regard this as a demonstration of the beneficial effect of the ITER-like wall configuration on the impurity species distribution in the JET divertor. The result is minimal tungsten sputtering at an effective sputter yield of  $< 10^{-4}$  for divertor temperatures below  $\sim 30$  eV.

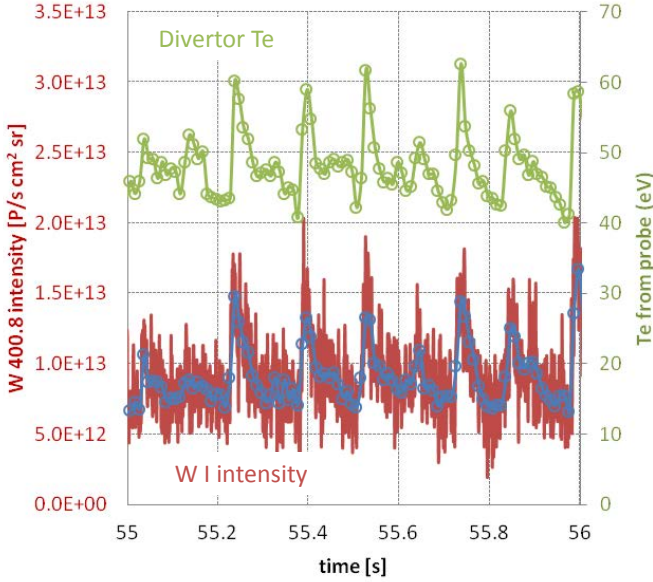


FIG. 4: Time traces of the divertor plasma temperature measured with Langmuir probes (upper signal, plotted against the right vertical axis) and the WI line radiation measured with a PMT (bottom signal against the left vertical axis) for discharge JPN 80896. The 20 eV temperature variations are promptly followed by the tungsten photon flux.

#### IV. EFFECT OF INCREASING THE BERYLLIUM CONTENT IN LOW DENSITY L-MODE DISCHARGES WITH LARGE SAWTEETH

After having established that beryllium is the dominant impurity with respect to tungsten sputtering, we investigated the dependence of the tungsten sputtering on both the beryllium flux and the divertor plasma conditions in a larger parameter range. For that reason, discharges with 1-3 MW ICRH auxiliary heating at medium to low line averaged plasma density ( $1.6 - 2.8 \times 10^{19} \text{ m}^{-3}$ ) were analyzed. Characteristic of these discharges were the strong oscillations in the divertor plasma temperature (and target flux density), which is illustrated by the time traces plotted in Fig. 4 for discharge JPN 80896. The upper trace is the oscillation in the divertor plasma temperature that was measured with Langmuir probes. The lower trace shows the raw as well as smoothed PMT measurement of the WI radiation at the strike point. The figure illustrates that the WI photon flux follows the temperature oscillations closely. This gives the opportunity to relate the instantaneous WI photon (or particle) fluxes and divertor conditions and evaluate again the effective erosion yields as a function of plasma temperature, i.e. energy of the sputtering particle. The results of this analysis is plotted in Fig. 5 for the discharges JPN80889, 80893, and 80896. It is seen that the increase of the tungsten sputtering with divertor temperature is similar as before, but also depended on the total heating power and on the main plasma density. The effect of the heating

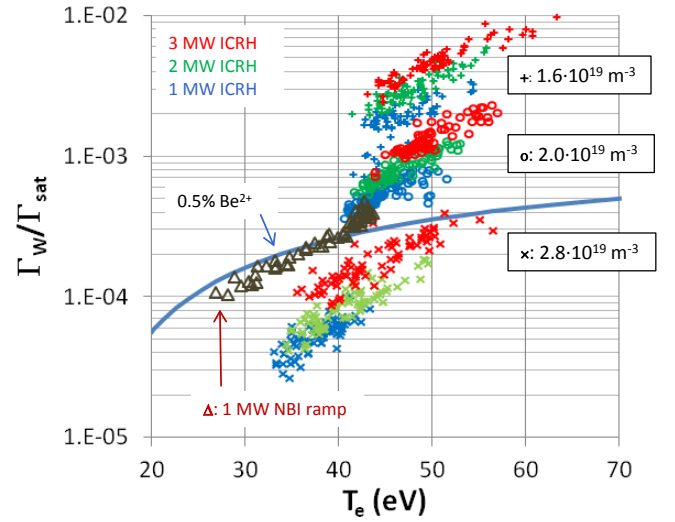


FIG. 5: Effective erosion yields determined from the sawteeth dominated ICRH discharges (JPN80889, 80893, 80896). The symbols refer to different main plasma densities, the colors refer to the different additional heating levels. For comparison, also the data from Fig. 3 are included.

power relates to an increasing Be content in the plasma and thus increasing Be influx in the divertor. Both the analysis of Z-effective of the main plasma and the BeII photon fluxes in the outer divertor indicate this. However, the observed increases in Z-effective did not account for the observed increase in tungsten sputtering at the lower densities. It presently remains unclear what effect is responsible. Possible effects playing a role here include uncertainties in the relation between the Langmuir probes temperature measurements and the impact energy of the sputtering particles, a plasma density dependence of the WI  $S/XB$  values, the appearance of other sputtering impurities or changes in the (non-coronal) charge state distributions.

#### V. ASSESSING PROMPT REDEPOSITION VIA WII SPECTROSCOPY

A consequence of the grazing angle incidence of the magnetic field with the divertor target is that most of the sputtered particles will return to the surface when the ionization mean free path of the sputtered tungsten atoms becomes smaller than the ion Larmor radius. This effect has first been discussed by Fussmann et al. [7]. Writing the redeposited fraction as

$$f_{\text{prompt}} = [1 + (\tau_{\text{ion}}\omega_c)^2]^{-1}, \quad (3)$$

and thereby assuming a  $\cos\theta$  angular velocity distribution of the sputtered atoms and correctly averaging over the distribution of ionization times for all ionization states allows to calculate the fraction as a function of divertor temperature and density. For a magnetic field of 2.0 T,



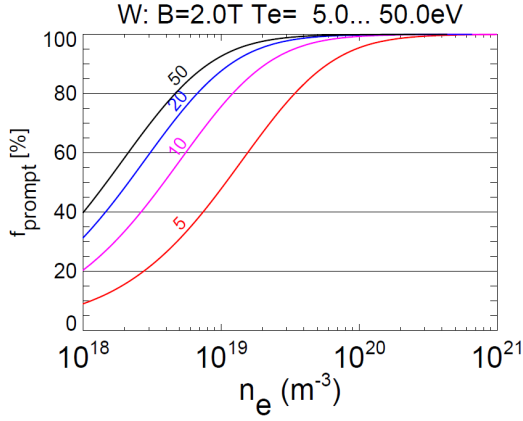


FIG. 6: Effective erosion yields determined from the sawteeth dominated ICRH discharges (JPN80889, 80893, 80896). The symbols refer to different main plasma densities, the colors refer to the different additional heating levels. For comparison, also the data from Fig. 3 are included.

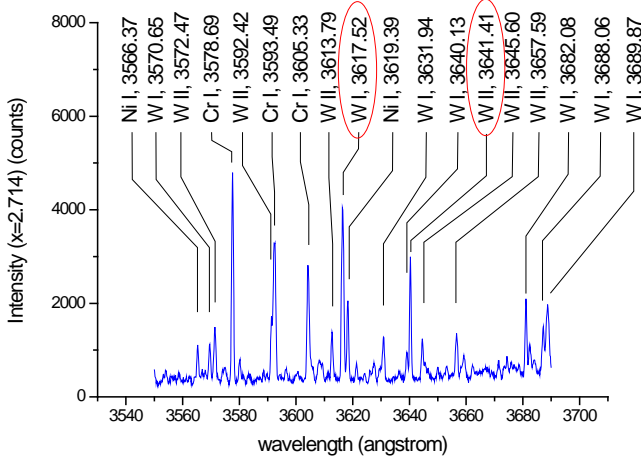


FIG. 7: Identification WI and WII lines in a UV spectrum recorded in discharge JPN 80896.

which was typical for the JET experiments discussed in the present, this resulted in the dependence plotted in Fig. 6. The plot shows that the redeposited fraction changes strongly at divertor densities of around  $10^{19} \text{ m}^{-3}$  given the temperature regime typical for the discharges discussed above, i.e.  $20 < T_e < 50 \text{ eV}$ .

A possible way to experimentally characterize the promptly redeposited fraction is by comparing spectral lines of neutral tungsten and ionized tungsten[8]. The rationale is that the  $S/XB$  for neutral tungsten lines is unaffected by redeposition "losses", whereas these do form an addition loss channel for ionized particles. Thus, assuming a redeposition rate  $R$ , the photon efficiency  $(S/XB)_{ion}$  transforms into  $((S + R)/XB)_{ion}$ .

Suitable WII lines are found in the UV, e.g. at 364 nm. A spectrum recorded in discharge JPN 80896 around that wavelength is shown in Fig. 7. In addition to the tungsten lines, also chromium and nickel lines are recog-

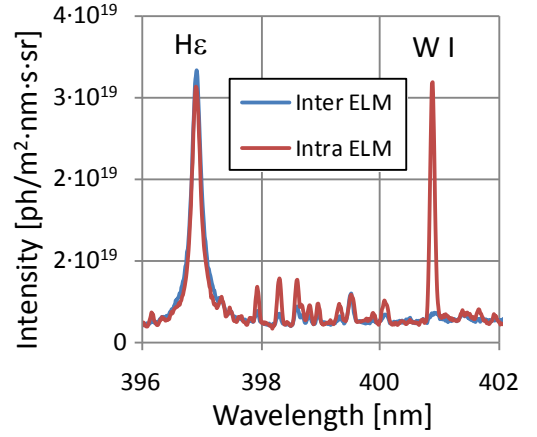


FIG. 8: Spectra recorded inter-ELM (blue) and intra-ELM (red) in discharge JPN 82237 illustrate that intra-ELM W sputtering is dominant (13 MW NBI,  $7.5 \times 10^{19} \text{ m}^{-3}$  line averaged  $n_e$ , 10 Hz ELMs).

nized, which originate from Incornel support structures throughout the main vessel. The two highlighted spectral lines were selected for the WII/WI line ratio analysis. The WI 361.7 nm line was selected on basis of its high intensity as well as strong correlation with the WI 400.9 nm line. The WII is obviously also for its intensity, but moreover as information on its  $S/XB$  values is available from modeling[9]. The line ratios were evaluated for the discharges JPN 80893 and 80896 around  $t = 60 \text{ s}$ , which means for divertor electron densities of  $1.2 \times 10^{19} \text{ m}^{-3}$  and  $0.4 \times 10^{19} \text{ m}^{-3}$ , respectively (measured by Langmuir probes at the strike point). The line ratio's were  $1.1 \pm 0.3$  and  $2.1 \pm 0.2$ , respectively (note the difference in relative accuracy due to the much lower line intensities at the higher plasma density). In other words, indeed a significant change is observed in the WII/WI line ratio. The factor of two change in the line ratio implies that the redeposition rate becomes larger than the ionization rate and thus more than half of the sputtered particles are redeposited.

## VI. TUNGSTEN SPUTTERING IN H-MODE: INTER- VERSUS INTRA-ELM SPUTTERING

The large difference between inter- and intra-ELM W sputtering in H-mode is illustrated by the spectra overlaid in Fig. 8. Obviously, as these spectra were recorded with the KT3 system, the time resolution was insufficient to resolve ELMs. Therefore, an example was chosen in which the ELM frequency was sufficiently low to record by coincidence spectra containing the contribution of one single ELM and spectra without any ELM contribution. The PMT measurements confirmed this for the spectra selected for the figure.

For this specific example, the inter-ELM sputtering amounted to  $9.7 \times 10^{18} \text{ atoms/s}$  (following from inte-

gration over the entire outer strike point). The inter-ELM total saturation current in the outer divertor was  $1.7 \times 10^{23}$  el/s, which means that the effective inter-ELM sputter yield amounted  $6 \times 10^{-5}$  and was thus similar to the L-mode sputter yields that were determined above. The intra-ELM sputtering was  $4.7 \times 10^{18}$  atoms/ELM. Given the 10 Hz ELM frequency, this means that intra-ELM sputtering dominated by a factor of 5 over inter-ELM sputtering.

## VII. NITROGEN SEEDING FOR CONTROLLING TUNGSTEN SPUTTERING

Extrinsic impurities may also be present as a result of impurity seeding to reduce power and energy loads on divertor targets (e.g. [10] and references therein). It is evident that, within the context of divertor target material sputtering, this involves a balance between increasing the impurity concentration due to the seeding on the one hand and decreasing the divertor plasma temperature to reduce the impact energy of the sputtering particle at the other hand. We illustrate this balance on the basis of a series of pulses (JPN 82293-82296: 1.1 MW NBI heating) in which nitrogen was seeded at different rates ( $4 \times 10^{21} - 1 \times 10^{22}$  el/s) in the divertor. The nitrogen flux to the target was monitored via the NIII 403.5 nm line. This signal is observed to build up during the discharge although the seeding level is being kept constant, a feature that is generally known for nitrogen seeding. The result is that the divertor plasma temperature decreases during the discharge. The lower panel in Fig. 9 shows the temperature decrease from initially 25 eV at the lowest seeding rate down to finally 5 eV at the highest seeding rate as a function of the NIII line intensity. The upper panel in the figure shows the tungsten particle flux determined from the WI line intensity as a function of the plasma temperature as it has been set by the nitrogen seeding. The plot confirms the expected trend. Starting from the highest temperatures, the tungsten sputtering increases steeply upon nitrogen seeding, evidently due to sputtering by nitrogen. In the present example the increase is a factor of three. The effect of plasma cooling starts to dominate around 20 eV, i.e. where the maximum sputtering is observed. The nitrogen seeding starts to have a net beneficial effect, i.e. a reduction in the tungsten erosion, when the temperature drops below 15 eV.

## VIII. CONCLUSIONS

The tungsten source in the outer divertor of JET in its ITER-like wall configuration, which is the region in which tungsten sputtering is maximum, has been quantified under various experimental conditions from spectroscopic

observation of the vertical target plate that consists of solid tungsten lamellae. We conclude that the erosion is

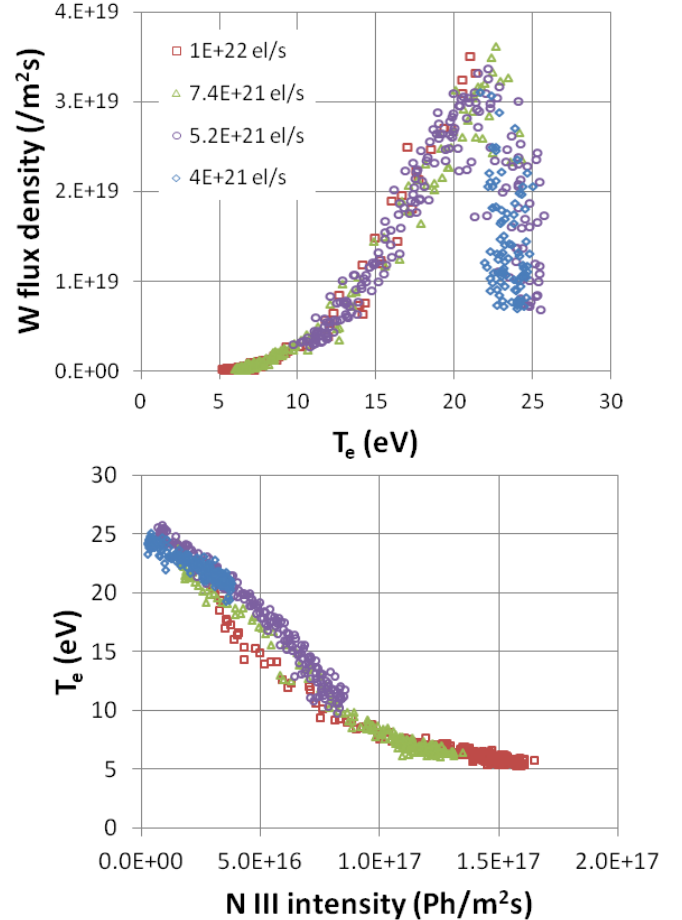


FIG. 9: Effect of nitrogen seeding in the divertor. The lower panel shows how the divertor plasma temperature drops as the nitrogen fluxes build up. The top panel shows that this leads initially to a steep increase in the tungsten sputtering due to higher concentrations impurities (i.e. nitrogen), whereafter plasma cooling takes over to decrease the sputtering.

mainly caused by beryllium, which is also the dominant impurity in the plasma. A rough estimate from spectroscopic signals indicates that the carbon fraction in the target flux is only 0.05%. In the one example studied in H-mode, it was confirmed that sputtering during ELMs dominates over in-between ELM sputtering. A calculation of the promptly redeposited tungsten fraction has been shown that predicts an order of magnitude lower *net* erosion, i.e. number of particle that really leave the target surface, compared to the *gross* erosion that has been characterized in the present. A first evaluation of the redeposited fraction has been performed by comparing neutral tungsten and tungsten ion lines, which confirms that prompt redeposition is significant.

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